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Unsteady three-dimensional MHD flow and mass transfer in a porous space in the presence of thermal radiation

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Unsteady three-dimensional MHD flow and mass transfer in a porous medium is presented here by taking into account of thermal radiation. The governing fundamental equations are first transformed into a system of ordinary differential equations using self similar transformation and they are solved numerically by using the sixth-order Runge-Kutta-Fehlberg method with shooting technique for some values of the physical parameters embedded in the flow model. Important features of the flow and heat transfer characteristic for different values of thermal radiation, magnetic field and chemical reaction are analyzed and discussed. Numerical results for the velocities, temperature and concentration profiles for a prescribed magnetic field, thermal radiation and chemical reaction parameters as well as the development of the local skin-friction coefficient, local Nusselt number and Sherwood number are reported graphically for various parametric conditions to show interesting aspect of the numerical solution.

Keywords: Unsteady flow: Three-dimensional stretching: Mass transfer: Porous medium: Radiation: Magnetic field.

INTRODUCTION

Boundary layer flow induced by a stretching surface has been studied extensively under varied conditions by many researchers because of its considerable engineering applications. For instance, aerodynamic extrusion of plastic sheets, cooling of metallic sheets in a cooling bath, in paper industry is few examples of such applications. Particularly, momentum and heat transfer in stretching flow of a viscoelastic fluid has been analyzed due to its ever increasing usage in manufacturing process of artificial film and artificial fibers. Literature survey establishes serious attention has been given to the steady two-dimensional flow bounded by a stretching surface whose velocity to the distance from a fixed origin varies linearly and nonlinearly. Some recent contributions on the topic have been presented (Cortell, 2007; Cortell, 2006; Liao, 2006; Liao, 2006; Ali, 2007; Xu, 2005; Kumari, 2009;

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Hayat, 2008; Sajid and Hayat, 2008; Sajid et al., 2008). Recently, Xu et al. (2007) looked at the unsteady threedimensional magnetohydrodynamic (MHD) boundary layer flow and heat transfer over a stretching sheet. They have presented the series solutions for the mathematical problems. Very recently, Hayat et al. (2010) studied homotopy solution for the unsteady three-dimensional MHD flow and mass transfer in a porous space.

Radiative heat transfer flow is very important in manufacturing industries for the design of reliable equipments, nuclear plants, gas turbines and various propulsion devices for aircraft, missiles, satellites and space vehicles. Similarly, the effects of thermal radiation on the forced and free convection flows are important in the content of space technology and processes involving high temperature. Based on these applications, England and Emery (1969) studied the thermal radiation effect of an optically thin gray gas bounded by a stationary vertical plate. Plumb et al. (1981) was the first to examine the effect of horizontal cross-flow and radiation on natural convection from vertical heated surface in saturated porous media. Rosseland diffusion approximation had been utilized in this investigation of convection flow with radiation. Makinde et al. (2011) examined unsteady convection with chemical reaction and radiative heat transfer past a flat porous plate moving through a binary mixture. Makinde and Olanrewaju (2011) studied unsteady mixed convection with Soret and Dufour effects past a porous plate moving through a binary mixture of chemically reacting fluid. Hayat et al. (2009) investigated the effect of thermal radiation on the flow of a second grade fluid and the references there in. Similarly, very recently, Hayat et al. (2010) studied effects of radiation and magnetic field on mixed convection stagnation-point flow over a vertical stretching sheet in a porous medium.

The aim of present work is to extend the analysis of Hayat et al. (2010) in three directions. This is because of the important in electrical power generation, astrophysical flows, solar power technology, space vehicle re-entry and other industrial areas. We present the problem formulation in Section 2. Section 3 includes the method of solutions. In Section 4, the solutions are analyzed by various parameters. Finally, main observations are presented in Section 5.

Mathematical formulation

We consider the transient and three-dimensional flow of a viscous fluid over a stretching surface. The fluid is electrically conducting in the presence of a constant applied magnetic field B_0 and thermal radiation. The induced magnetic field is neglected under the assumption of a small magnetic Reynolds number. Initially (for t=0), both fluid and plate are stationary and they have constant temperature $T_{..}$ and Concentration C_{∞} . The plate at t=0 is expressed by the velocity components u = ax, v = by (u and v are the velocity components in x- and y-directions). Now, for this time the surface temperature and concentration vary from T_{∞} to T_{w} and C_{∞} to C_{w} , respectively. The mathematical statements for the boundary layer problem are 2

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \qquad (1)$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = v \frac{\partial^2 u}{\partial z^2} - \frac{\sigma B_0^2}{\rho} u - \frac{v \varphi}{k'} u, \quad (2)$$
$$\frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = v \frac{\partial^2 v}{\partial z^2} - \frac{\sigma B_0^2}{\rho} v - \frac{v \varphi}{k'} v, \quad (3)$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \alpha \frac{\partial^2 T}{\partial z^2} - \frac{\alpha}{k} \frac{\partial q_r}{\partial z}, \qquad (4)$$

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} + w \frac{\partial C}{\partial z} = D \frac{\partial^2 C}{\partial z^2} - k_1 C, \qquad (5)$$

where *w* is the z-component of velocity, ρ is the fluid density, v is the kinematic viscosity, σ is the electrical conductivity, φ is the porosity, k' is the permeability of the porous medium, *C* is the concentration species of the fluid, *D* is the diffusion coefficient of the diffusion species in the fluid, k_1 is the first-order homogeneous constant reaction rate and α is the thermal diffusivity. The corresponding boundary conditions are

$$u = v = w = 0, \ T = T_{\infty}, \ C = C_{\infty}, \ t < 0$$

$$u = u_{w} = ax, \ v = v_{w} = by, \ w = 0, \ T = T_{w}, \ C = C_{w}, \ z = 0; \ t \ge 0,$$

$$u \to 0, \ v \to 0, \ T \to 0, \ C \to 0, \ as \ z \to \infty; \ t \ge 0,$$
(6)

where the constants a and b are positive. The radiative heat flux q_r is described by Roseland approximation (Sajid et al. (2008)) such that

$$q_r = -\frac{4\sigma^*}{3K}\frac{\partial T^4}{\partial y},\tag{7}$$

where σ^* and K are the Stefan-Boltzmann constant and the mean absorption coefficient, respectively. Following Sajid and Hayat, (2008), we assume that the temperature differences within the flow are sufficiently small so that T^4 can be expressed as a linear function after using Taylor series to expand T^4 about the free stream temperature T_{∞} and neglecting higher-order terms. This results in the following approximation:

$$T^4 \approx 4T_{\infty}^3 T - 3T_{\infty}^4$$
. (8)

Using (8) and (7) in (4), we obtain

$$\frac{\partial q_r}{\partial y} \approx -\frac{16\sigma^* T_{\infty}^3}{3K} \frac{\partial^2 T}{\partial y^2}.$$
 (9)

Following Hayat et al., (2011), it is convenient to use the following similarity transformations:

$$\eta = \sqrt{\frac{a}{v\varepsilon}} z, \quad \varepsilon = 1 - \exp(-\tau), \quad \tau = at, \quad u = ax \frac{\partial f}{\partial \eta}, \quad v = ay \frac{\partial g}{\partial \eta}, \quad w = -\sqrt{av\varepsilon}(f+g),$$

$$\theta = \frac{T - T_{\infty}}{T_w - T_{\infty}}, \qquad \phi = \frac{C - C_{\infty}}{C_w - C_{\infty}}.$$

(10)

Eq. (1) is satisfied identically and Eqs. (2)-(5) becomes

$$f''' + (1 - \varepsilon) \left(\frac{\eta}{2} f'' - \varepsilon \frac{\partial f'}{\partial \varepsilon} \right) + \varepsilon \left[(f + g) f'' - (f')^2 - M^2 f' - \lambda f' \right] = 0,$$
(11)

$$\begin{split} g''' + (1-\varepsilon) & \left(\frac{\eta}{2}g'' - \varepsilon \frac{\partial g'}{\partial \varepsilon}\right) + \varepsilon \Big[(f+g)g'' - (g')^2 - M^2g' - \lambda g' \Big] = 0, \\ (12) \\ \theta'' \Big[1 + \frac{4}{3}Ra \Big] + \Pr(1-\varepsilon) & \left(\frac{\eta}{2}\theta' - \varepsilon \frac{\partial \theta}{\partial \varepsilon}\right) + \Pr\varepsilon(f+g)\theta' = 0, \\ (13) \\ \theta'' + Sc(1-\varepsilon) & \left(\frac{\eta}{2}\phi' - \varepsilon \frac{\partial \phi}{\partial \varepsilon}\right) + Sc\varepsilon(f+g)\phi' - \gamma Sc\varepsilon\phi = 0, \\ (14) \\ f(\varepsilon,0) = g(\varepsilon,0) = 0, f'(\varepsilon,0) = \theta(\varepsilon,0) = \phi(\varepsilon,0) = 1, g'(\varepsilon,0) = c, \\ f'(\varepsilon,\infty) = g'(\varepsilon,\infty) = \theta(\varepsilon,\infty) = \phi(\varepsilon,\infty) = 0. \\ (15) \end{split}$$

Prime denotes the derivative with respect to η , c (= b/a) the stretching parameter is a positive constant. It was noted that when c = 0, the problem reduces to twodimensional case. Here the local Hartman number M, the local porosity parameter λ , the Schmidt number Sc, the chemical reaction parameter γ and the thermal radiation parameter *Ra* are given by

$$M^{2} = \frac{\sigma B_{0}^{2}}{\rho a}, \ \lambda = \frac{\upsilon \varphi}{ak}, \ \Pr = \frac{\upsilon}{a}, \ Sc = \frac{\upsilon}{D}, \ \gamma = \frac{k_{1}}{a}, \ Ra = \frac{4\alpha \sigma^{*} T_{\infty}^{3}}{K' k}.$$
(16)

Here, the skin friction coefficients C_{fx} and C_{fy} in x- and y-directions, local Nusselt number Nu and local Sherwood number Sh are

$$\operatorname{Re}_{x}^{\frac{1}{2}} \varepsilon^{\frac{1}{2}} C_{fx} = -f''(\varepsilon,0), \quad \operatorname{Re}_{y}^{\frac{1}{2}} \varepsilon^{\frac{1}{2}} C_{fy} = -g''(\varepsilon,0),$$
$$\operatorname{Nu}\operatorname{Re}_{x}^{-\frac{1}{2}} \varepsilon^{\frac{1}{2}} = -\theta'(\varepsilon,0), \quad Sh\operatorname{Re}_{x}^{-\frac{1}{2}} \varepsilon^{\frac{1}{2}} = -\phi'(\varepsilon,0),$$
(17)

where $Re_x = ax^2/v$ and $Re_v = ay^2/v$ are the local Reynolds number, $f''(\varepsilon,0)$ and $g''(\varepsilon,0)$ are the surface shear stresses in x- and y-directions, $\theta'(\varepsilon,0)$ is the surface heat transfer parameter and $\phi'(\varepsilon,0)$ is the surface mass transfer parameter.

For $\varepsilon = 0$, Eqs. (11)-(14) can be written as

$$f''' + \frac{\eta}{2} f'' = 0,$$

$$g''' + \frac{\eta}{2} g'' = 0,$$

$$[1 + \frac{4Ra}{3}]\theta'' + \Pr\frac{\eta}{2}\theta' = 0,$$

$$\phi'' + Sc\frac{\eta}{2}\phi' = 0.$$
Similarly for $s = 1$ Eqs. (11)-(14) becomes

Similarly for $\mathcal{E} = I$, Eqs. (11)-(14) becomes

$$f''' + (f + g)f'' - f'^{2} - M^{2}f' - \lambda f' = 0,$$

$$g''' + (f + g)g'' - g'^{2} - M^{2}g' - \lambda g' = 0,$$

$$[1 + \frac{4Ra}{3}]\theta'' + \Pr(f + g)\theta' = 0,$$

$$\phi'' + Sc(f + g)\phi' - \gamma Sc\phi = 0,$$
(19)

subject to the boundary conditions (15).

Method of Solution

Here, we solve Eqs. (18) analytically and Eqs. (19) numerically using Shooting technique with sixth order Runge-Kutta method. It can be seen that for $\varepsilon = 0$, Eq. (18) has a closed form solution of the form

$$f(0,\eta) = \eta \operatorname{erfc}\left(\frac{\eta}{2}\right) + \frac{2}{\sqrt{\pi}} \left[1 - \exp\left(-\frac{\eta^2}{4}\right)\right],$$

$$g(0,\eta) = c \left(\eta \operatorname{erfc}\left(\frac{\eta}{2}\right) + \frac{2}{\sqrt{\pi}} \left[1 - \exp\left(-\frac{\eta^2}{4}\right)\right]\right),$$

$$\theta(0,\eta) = \operatorname{erfc}\left(\frac{\left(\sqrt{\frac{3\operatorname{Pr}}{3 + 4\operatorname{Ra}}}\right)}{2}\eta\right),$$

$$\phi(0,\eta) = \operatorname{erfc}\left(\frac{\sqrt{\operatorname{Sc}}}{2}\eta\right),$$

(20)

where

$$erfc(\eta) = 1 - \frac{2}{\sqrt{\pi}} \int_{0}^{\eta} \exp(-x^2) dx.$$
 (21)

Eq. (19) constitutes a highly non-linear coupled boundary value problem of third and second-order. So we develop most effective numerical shooting technique with sixth-order Runge-Kutta integration algorithm. To select η_{∞} we begin with some initial guess value and solve the problem with some particular set of parameters to obtain $f''(\varepsilon,0), g''(\varepsilon,0), \theta'(\varepsilon,0)$ and $\phi'(\varepsilon,0)$. The solution process is repeated with another larger value of $\eta_{\rm m}$ until successive values of two $f''(\varepsilon,0), g''(\varepsilon,0), \theta'(\varepsilon,0)$ and $\phi'(\varepsilon,0)$ differ only after desired digits signifying the limit of the boundary along η . The last value of η_{∞} is chosen as appropriate value for that particular simultaneous equations of first order for seven unknowns following the method of superposition. To solve this system we require ten initial

М	Sc	Dr	Ba	Å	V	<u>^</u>	f''(z,0)	$-''(a_0)$	O'(a 0)	$\phi'(a,0)$
101	00		na	Λ	Y	C	$-f(\mathcal{E},0)$	$-g(\mathcal{E},0)$	$-\theta(\varepsilon,0)$	$-\psi(\varepsilon,0)$
0	1	1	1	1	1	0.1	1.42707425	0.11989595	0.28417669	1.17092198
0.1	1	1	1	1	1	0.1	1.43056719	0.12031101	0.28378656	1.17074353
0.3	1	1	1	1	1	0.1	1.45821203	0.12358193	0.28074425	1.16934359
0.4	1	1	1	1	1	0.1	1.48198158	0.12637529	0.27819159	1.16815717
0.1	0.62	1	1	1	1	0.1	1.43056719	0.12031101	0.28378656	0.90796272
0.1	0.78	1	1	1	1	0.1	1.43056719	0.12031101	0.28378656	1.02595318
0.1	2.62	1	1	1	1	0.1	1.43056719	0.12031101	0.28378656	1.94693909
0.1	1	0.72	1	1	1	0.1	1.43056719	0.12031101	0.22732899	1.17074353
0.1	1	3.00	1	1	1	0.1	1.43056719	0.12031101	0.64411898	1.17074353
0.1	1	7.10	1	1	1	0.1	1.43056719	0.12031101	1.15093985	1.17074353
0.1	1	1	1	1	1	0.1	1.43056719	0.12031101	0.28378656	1.17074353
0.1	1	1	2	1	1	0.1	1.43056719	0.12031101	0.21079238	1.17074353
0.1	1	1	3	1	1	0.1	1.43056719	0.12031101	0.17818658	1.17074353
0.1	1	1	1	0.1	1	0.1	1.07235304	0.07445359	0.33135495	1.19109626
0.1	1	1	1	0.3	1	0.1	1.16132221	0.08668680	0.31800509	1.18562015
0.1	1	1	1	0.4	1	0.1	1.20341226	0.09222260	0.31206396	1.18313408
0.1	1	1	1	1	0.1	0.1	1.43056719	0.12031101	0.28378656	0.63711465
0.1	1	1	1	1	0.3	0.1	1.43056719	0.12031101	0.28378656	0.79351784
0.1	1	1	1	1	0.4	0.1	1.43056719	0.12031101	0.28378656	0.85919188
0.1	1	1	1	1	1	0.00	1.41774468	0.00000000	0.26665579	1.15485136
0.1	1	1	1	1	1	0.25	1.44945710	0.31642983	0.30811892	1.19400515
0.1	1	1	1	1	1	0.50	1.48012872	0.68163040	0.34556949	1.23142220

Table 1. Values of $f''(\mathcal{E},0), g''(\mathcal{E},0), \theta'(\mathcal{E},0)$ and $\phi'(\mathcal{E},0)$ for the embedded flow parameters in the flow model when $\varepsilon = 1$.

conditions whilst we have only two initial conditions. Now, we employ numerical shooting technique where these two ending boundary conditions are utilized to produce two unknown initial conditions at $\eta = 0$. In this calculation, the step size $\Delta \eta = 0.001$ is used while obtaining the numerical solution with $\eta_{\rm max} = 11$ and five-decimal accuracy as the criterion for convergence.

RESULTS AND DISCUSSION

Numerical calculations have been carried out for different values of the thermophysical parameters controlling the fluid dynamics in the flow regime. The values of Schmidt number (*Sc*) are chosen as water vapour (*Sc* = 0.62), ammonia (*Sc* = 0.78) and Propyl Benzene (*Sc* = 2.62) at temperature 25°C and one atmospheric pressure. The value of Prandtl number was chosen to be Pr = 0.72 which represents air at temperature 25°C and one atmospheric pressure. In all computation we desire the variation of *f*, *g*, θ and ϕ versus η for the velocities, temperature and species diffusion boundary layers. Table (1) shows the computations for the influence of the embedded flow parameters on the local skin friction on *x* and *y*

directions together with the heat and mass transfer rate at the moving plate surface. It is quite interesting to note that increase in Sc. and y has no effects on the skin friction coefficients and the Nusselt number at the surface $f''(\varepsilon,0), g''(\varepsilon,0)$ and $\theta'(\varepsilon,0)$ but increases the Sherwood number at the surface boundary laver. Skin friction coefficients at the surface increases as the Hartman number increases. It was also seen that the skin friction coefficients increases with an increase in the porosity parameter and at the same time decreasing the Nusselt and Sherwood number at the surface. Significantly. the radiation parameter Ra has appreciable influence on the heat transfer rate but with no effect on the other interesting physical quantities since it was only involved in the temperature equation. It was established from the table that as thermal radiation parameter Ra increases, the heat transfer rate decreases. It is noteworthy to note that the stretching parameter c has greater influence on the physical properties of the flow. It was seen clearly that increase in parameter c increases the skin friction coefficients, the Nusselt and Sherwood numbers at the surface boundary layer $f''(\varepsilon,0), g''(\varepsilon,0), \theta'(\varepsilon,0)$ and $\phi'(\varepsilon,0)$. It is interesting to note that positive value of y represents destructive and negative values represent generative chemical reaction. Increasing parameter γ



Figure 1. Velocity profiles for Ra = 1, Sc = 1, c = 0.5, ϵ = 1, λ = 0.5, Pr = 1, γ = 1.



Figure 2. Velocity profiles for Pr = 1, M = 1, c = 0.5, ϵ = 1, Ra = 0.5, Sc = 1, γ = 1.

increases the Sherwood number at the surface.F

Velocity Profiles

Figures 1-6 depict the effects of emerging flow parameters on non-dimensional velocity profiles. In figure 1, the effect of increasing the Hartman number on the momentum boundary-layer thickness is illustrated. Increasing this parameter lead to a decrease in the velocity which confirmed with the fact that the magnetic field presents a damping effect on the velocity by creating a drag force that opposes the fluid motion. Figure 2 shows a decrease in the fluid velocity within the boundary layer due to porosity parameter. This indicates the usual fact that porosity stabilizes the boundary layer growth. Furthermore, figure 3 shows that an increase in the stretching parameter leads to a small decrease in the velocity profile. Figure 4-6 has similar effect with Figures 1-3 as expected.

Temperature Profiles

The effects of various thermophysical parameters on the fluid temperature are illustrated in Figures 7 to 11.

In figure 7, we observed that an increase in the Hartman number enhances the thermal boundary layer thickness. Figure 8 shows the influence of Prandtl number on fluid temperature. Physically, as the Prandtl number is a ratio of viscous to thermal diffusion, increase in Prandtl number indicates a decrease in thermal diffusion, and hence decreases the thermal boundary layer thickness. Figure 9 depicts the graph of temperature against spanwise coordinate η for various values of thermal radiation parameter. Due to radiation absorption the thermal boundary layer thickness increases as the radiation parameter increases. It is interesting to note that increase in the porosity parameter increases the temperature boundary layer thickness (see figure 10). Figure 11 represents the temperature solution for various values of the stretching



Figure 3. Velocity profiles for Pr = 1, M = 1, γ = 0.5, ϵ = 1, Ra = 0.5, Sc = 1, λ = 1.



Figure 4. Velocity profiles for Ra = 1, Sc = 1, c = 0.5, ϵ = 1, λ = 0.5, Pr = 1, γ = 1.



Figure 5. Velocity profiles for Pr = 1, M = 1, c = 0.5, ϵ = 1, Ra = 0.5, Sc = 1, γ = 1.



Figure 6. Velocity profiles for Pr = 1, M = 1, γ = 0.5, ϵ = 1, Ra = 0.5, Sc = 1, λ =1



Figure 7. Temperature profiles for Ra = 1, Sc = 1, c = 0.5, ϵ = 1, λ = 0.5, Pr = 1, γ = 1.



Figure 8. Temperature profiles for Ra = 1, M = 1, c = 0.5, ϵ = 1, λ = 0.5, Sc = 1, γ = 1.

parameter c. It was noticed that the thermal boundary layer thickness decreases as the stretching parameter c increases across the plate.

Concentration Profiles

Figures 12–15 depict the fluid concentration profiles against spanwise coordinate η for varying values of physical parameters in the boundary layer. Figure 12 shows the influence of the magnetic field parameter M on the species concentration. Increasing the Hartman number increases the species concentration boundary layer thickness. Figure 13 described the influence of

CONCLUSIONS

This present article discusses a mathematical model for the transient flow with heat and mass transfer in the presence of thermal radiation. Three dimensional stretching cases have been taken care off. Closed form solutions are first developed for $\varepsilon = 0$. For $\varepsilon = 1$, numerical solutions were obtained and interpreted for different involved embedded flow parameters. The following conclusions were drawn as follows:

• The effects of Hartman number and the porosity parameter are qualitatively similar.

• The effect of decreasing values of M and λ is to increase the boundary layer thickness.

• The effect of Schmidt number *Sc* is to decrease the concentration boundary layer thickness

• The effect of radiation parameter *Ra* is to increase the thermal boundary layer thickness through absorption.

• The thermal boundary layer thickness increases as Prandtl number *Pr* decreases.

• The influence of c and M on the skin friction coefficients are the same.

• The effect of the destructive chemical reaction parameter γ is to reduce the concentration field.

• The radiation parameter *Ra* has no effect on the skin friction coefficients and the mass transfer rate as expected.

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Schmidt number on the species concentration and it was observed that increase in Schmidt number leads to a decrease in the species concentration within the boundary layer due to the combined effects of buoyancy forces and species molecular diffusivity. Moreover, it is noteworthy that increasing values of chemical reaction parameter decreases the species concentration boundary layer thickness as illustrated in figure 14. Finally, it is noteworthy to note that increasing the ratio of stretching constant c decreases the species concentration boundary layer thickness across the plate.

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